

CORE ANALYSIS REPORT

PENNZOIL COMPANY  
J. V. R. SKINNER NO. 20 WELL  
KANAWHA COUNTY, WEST VIRGINIA

039 3409

7507 STEMMONS FRELWAY, BOX 47347, DALLAS, TEXAS 75247-2147/631-8270  
CORE LABORATORIES, INC.



P. O. Box 131  
Mt. Pleasant, Mich. 48858

Pennzoil Company  
P. O. Drawer 1588  
Parkersburg, W. Va. 26101

File No: 3602-487  
July 5, 1979

Att: Mr. George P. SanFilippo

Re: Core Analysis Report  
Wier Sandstone Formation  
J. V. R. Skinner No. 20 Well  
Blue Creek-Skinner Field  
Kanawha County, West Virginia

Gentlemen:

A diamond core from this well between the depths of 1731 feet and 1775 feet has been received in our Michigan laboratory. The following analyses have been performed on this core in accordance with your letter of June 7, 1979:

1. Grain density and whole core porosity.
2. Vertical whole core permeability determinations on 1' intervals. Vertical plug permeability was run if the samples were too small for vertical whole core permeabilities.
3. Horizontal plug permeability on 1' intervals of the core. All plug samples taken from the center of the core.
4. 90° plug permeability on 1' intervals of the core as close as possible to the same plane as the above plug.
5. Fluid saturations on 1' intervals.

Results of these analyses are herein submitted in tabular form.

The core will be returned to your office via motor freight. The opportunity to be of service on this well is appreciated and please call if you have any questions.

Very truly yours,

CORE LABORATORIES, INC.

A handwritten signature in cursive script that reads "Mabre Maness".

Mabre Maness, District Manager

er  
encl.

CORE LABORATORIES, INC.  
 Petroleum Reservoir Engineering  
 DALLAS, TEXAS

PENNZOIL COMPANY  
 J. V. SKINNER NO. 20 WELL  
 BLUE CREEK-SKINNER FIELD  
 KANAWHA COUNTY, W.VA.

JUNE 11, 1979  
 FILE NO. 3602-487  
 ANALYST: REINHEIMER

WIER SANDSTONE FORMATION

FULL DIAMETER ANALYSIS

SMP. NO.	DEPTH	GRN. DNS.	POROSITY GEX	PERMEABILITY DATA			FLUID SATURATIONS		DESCRIPTION
				FULL DIAMETER		PLUG	OIL	WATER	
				VERT.	0°	90°	%P.V.	%P.V.	
1	1737.1-38	2.68	8.2	0.6	1.5	1.6	16.1	10.9	SS
2	1738-39	2.66	7.2	<0.1	0.8	0.2	21.8	14.6	SS
3	1739-40	2.67	8.2	0.3	0.6	0.6	21.7	15.1	SS
4	1740-41	2.67	8.6	0.4	0.6	1.0	21.8	15.2	SS
5	1741-42	2.67	8.3	0.6	1.9	1.0	19.3	11.2	SS
6	1742-43	2.67	7.8	0.1	1.0	1.0	20.3	11.9	SS
7	1743-44	2.68	9.3	0.7	1.3	1.7	20.9	12.7	SS
8	1744-45	2.69	8.3	0.3	0.4	0.4	23.3	14.1	SS
9	1745-46	2.65	7.9	0.3	1.3	1.3	18.2	12.4	SS, SL/SHLY
10	1746-47	2.68	12.7	<0.1	1.5	3.5	29.0	18.5	SS
11	1747-48	2.74*	8.9	<0.1	*	0.6	25.7	16.9	SS, SHLY
12	1748-49	2.67	11.3	0.1	0.6	0.6	23.0	16.1	SS
13	1749-50	2.76*	13.8	<0.1	*	0.2	23.4	16.6	SS
14	1750-51	2.66	14.7	0.3		26	23.0	16.1	SS
15	1751-52	2.69	10.1	<0.1	0.4	0.4	20.8	18.1	SS
16	1752-53	2.66	8.1	0.3	0.6	0.6	18.5	16.2	SS
17	1753-54	2.67	7.4	<0.1	0.2	0.2	20.9	18.2	SS
18	1754-55	2.65	7.1	<0.1	0.2	0.2	13.2	16.5	SS, SL/SHLY
19	1755-56	2.64	7.1	<0.1	0.2	0.2	15.9	19.7	SS, SL/SHLY
20	1756-57	2.66	7.6	<0.1	0.6	0.2	15.5	18.7	SS
21	1757-58	2.66	7.6	<0.1	0.8	0.8	14.4	17.5	SS
22	1758-59	2.67	7.5	0.5	0.8	0.8	18.5	13.4	SS

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**CORE LABORATORIES, INC.**  
 Petroleum Reservoir Engineering  
 DALLAS, TEXAS

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FULL DIAMETER ANALYSIS

SMP. NO.	DEPTH	GRN. DNS.	POROSITY GEX	PERMEABILITY DATA			FLUID SATURATIONS		DESCRIPTION
				FULL DIAMETER VERT.	PLUG		OIL %P.V.	WATER %P.V.	
					0°	90°			
23	1759-60	2.66	7.0	0.3	1.3	0.4	23.4	17.0	SS
24	1760-61	2.66	8.7	0.1	0.4	0.3	20.2	14.8	SS
25	1761-62	2.66	8.4	0.3	0.8	0.6	15.9	16.3	SS
26	1762-63	2.66	7.0	<0.1	0.4	<0.1	17.8	18.2	SS
27	1763-64	2.65	8.5	0.2	0.4	0.6	19.9	18.8	SS
28	1764-65	2.65	8.5	1.1	1.9	2.1	15.7	14.6	SS
29	1765-66	2.66	8.8	0.8	1.7	2.1	17.2	16.0	SS
30	1766-67	2.62	9.6	1.5	2.5	3.3	17.2	16.0	SS, SHLY
31	1767-68	2.65	8.0	0.4	0.6	0.8	18.0	17.0	SS, SL/SHLY
32	1768-69	2.67	9.5	0.4	1.0	4.4	23.1	30.8	SS
33	1769-70	2.67	11.8	1.4	80	21	14.7	19.6	SS
34	1770-71	2.68	9.2	1.4	1.7	1.7	18.9	25.0	SS
35	1771-72	2.67	22.5	409	1157	1683	9.0	18.0	SS
36	1772-73	2.68	15.0	0.5	15	11	16.7	33.4	SS
37	1773-74	2.65	24.5	514	1052	2987	11.8	23.6	SS
38	1774-74.7	2.70*	11.8	<0.1	*	4.4	12.7	25.1	SS, SL/SHLY

(A)  $S_w = 212$

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