

75

RP=675# 4700700937

WELL NO. 11244  
SAND Big Tiger

LOG INTERPRETATION

①

| DEPTH | DENSITY |      | R <sub>f</sub> | NEUTRON |    |    |    | CORE |    |   | LOG |    |    |    | PERFORATING DEPTH |
|-------|---------|------|----------------|---------|----|----|----|------|----|---|-----|----|----|----|-------------------|
|       | C/SEC   | BULK |                | INDEX   | Øt | Sw | So | So   | Sw | Ø | Ø   | Sw | Sg | So |                   |
|       | RMA =   |      | 2.75           |         |    |    |    |      |    |   |     |    |    |    |                   |
| 1888  | 2.51    | 25   | 25             |         |    |    |    |      |    |   | 106 | 42 |    |    | 8 <sup>a</sup>    |
| 89    | 2.46    | 25   | 25             |         |    |    |    |      |    |   | 12  | 38 |    |    |                   |
| 90    | 2.44    | 25   | 25             |         |    |    |    |      |    |   | 125 | 35 |    |    | 10                |
| 91    | 2.40    | 25   | 25             |         |    |    |    |      |    |   | 14  | 31 |    |    | HOLES             |
| 92    | 2.40    | 25   | 25             |         |    |    |    |      |    |   | 14  | 31 |    |    |                   |
| 93    | 2.47    | 25   | 25             |         |    |    |    |      |    |   | 115 | 39 |    |    | 23                |
| 1876  | 2.51    | 30   | 30             |         |    |    |    |      |    |   | 95  | 40 |    |    | 16                |
| 97    | 2.47    | 40   | 40             |         |    |    |    |      |    |   | 11  | 31 |    |    | 8                 |
| 98    | 2.40    | 50   | 50             |         |    |    |    |      |    |   | 14  | 21 |    |    | HOLES             |
| 99    | 2.40    | 50   | 50             |         |    |    |    |      |    |   | 14  | 21 |    |    |                   |
| 1700  | 2.40    | 50   | 50             |         |    |    |    |      |    |   | 14  | 21 |    |    | 01                |
| 01    | 2.46    | 40   | 40             |         |    |    |    |      |    |   | 115 | 30 |    |    |                   |

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West. = RT  
67517M

$$43560 \times \frac{723}{(460 + 60)} \times \frac{.849 \times 15.325 \times (460 + 75)}{375,960} \times \frac{110}{67517} \text{ Ac.} =$$

$$54.0$$

|      |             |        |       |                   |         |     |
|------|-------------|--------|-------|-------------------|---------|-----|
| 1888 | 258,746,400 | X .10  | X .58 | =                 | 15,007  | MCF |
| 89   |             | X .12  | X .62 | =                 | 19,251  |     |
| 90   |             | X .125 | X .65 | =                 | 21,023  |     |
| 91   |             | X .14  | X .69 | =                 | 49,990  |     |
| 92   |             | X .14  | X .69 | } <sup>2'</sup> = | —       |     |
| 1893 |             | X .115 | X .61 | =                 | 18,151  |     |
| 1896 |             | X .095 | X .60 | =                 | 14,749  |     |
| 97   |             | X .11  | X .69 | =                 | 19,639  |     |
| 98   |             | X .14  | X .79 | =                 | —       |     |
| 99   |             | X .14  | X .79 | } <sup>3'</sup> = | 85,252  |     |
| 00   |             | X .14  | X .79 | =                 | —       |     |
| 1901 |             | X .115 | X .70 | =                 | 20,829  |     |
|      |             |        |       |                   | 264,491 | MC  |

250

11/17

GL =  $.706 \times 1895 = 1342$

Wellhead \* =  $675 + 15 = 690$

Res. Press. 723

Cv. =  $.708^E$

Per. = 668

Ter. = 394

Pr. =  $\frac{723}{668} = 1$

Tr. =  $\frac{535}{394} = 1$

Z =  $.849$